

# PN-EMISSIONS WITH INCREASED LUBE OIL CONSUMPTION OF GDI CAR WITH/WITHOUT GPF

**Jan Czerwinski, Pierre Comte, Martin Güdel**

*AFHB Laboratory for Exhaust Emission Control of the Berne University of Applied Science,  
Biel/Bienne, Switzerland  
tel. +41 32 3216680  
e-mail: [jan.czerwinski@bfh.ch](mailto:jan.czerwinski@bfh.ch), [pierre.comte@bfh.ch](mailto:pierre.comte@bfh.ch), [martin.güdel@bfh.ch](mailto:martin.güdel@bfh.ch)*

**Markus Kurzwart**

*Motorex, Langenthal, Switzerland  
tel. +41 62 919 76 74  
e-mail: [markus.kurzwart@motorex.com](mailto:markus.kurzwart@motorex.com)*

**Andreas Mayer**

*TTM, Technik Thermische Maschinen, Niederrohrdorf, Switzerland  
Tel. +41 56 496 64 14, fax: +41 56 496 64 15  
e-mail: [ttm.a.mayer@bluewin.ch](mailto:ttm.a.mayer@bluewin.ch)*

## **Abstract**

*The particle number (PN) emissions are increasingly considered in the progressing exhaust gas legislation for on- and off- road vehicles. The invisible nanoparticles penetrate like a gas into the living organisms and cause several health hazards.*

*The present paper shows how the PN- and gaseous emissions of a modern GDI \*) vehicle change, when there is an in-creased lube oil consumption. What are the potentials of a gasoline particle filter to reduce the emissions?*

*The lube oil consumption was simulated by mixing 2% vol. lube oil into the fuel. A non-coated GPF was mounted at tailpipe, so only the filtration effects were indicated.*

*The tests were performed at transient (WLTC) and at stationary (SSC) operating conditions.*

*It has been shown that the increased lube oil consumption significantly increases the PN-emissions and the applied high quality GPF eliminates these emissions very efficiently.*

**Keywords:** *PN-emissions of road transport, combustion engines, air pollution, environmental protection*

## **1. Introduction**

The nanoaerosol in vehicle exhaust is known to be a complex mixture of different volatile and non-volatile species often showing a bi-modal particle size distribution with a nucleation mode smaller than 20 nm and a larger accumulation mode that mainly contains aggregates of primary particles.

The larger accumulation mode is usually composed of more graphitic soot particles with an elemental carbon (EC) structure, whereas the particles in the nucleation mode are reported to be mainly volatile organics, especially when sulphur is absent from fuel and lubrication oil, [1-4]. However, recent studies detected also low-volatility particle fractions in the ultrafine size range when sampling was carried out according to PMP protocol at 300 °C, [5-7].

---

\*) Abbreviations see at the end of this paper

These particles are suspected to be nucleated metal oxides originating from metal additives in lubrication oil or fuels [8-11]. The formation of this particulate fraction was especially observed when the soot content was low as in idle condition of diesel vehicles. These particles mainly appear in the ultrafine size range <23 nm. While the mass contribution of these ultrafine particles in vehicle emissions is very low, their contribution to the number concentration is significant.

Studies for gasoline fuelled internal combustion engines pointed out that also this vehicle class can emit remarkable amounts of particles, [6, 12, 13]. Especially gasoline direct injection technology (GDI) shows particle number (PN) emissions significantly higher than modern diesel cars equipped with best available DPF technology.

The nanoparticles emissions are produced especially at cold start and warm-up conditions and at a dynamic engine operation, [14]. The lube oil contributes to this emission in the sense of number concentrations in nuclei mode and composition, [8, 9, 10].

The investigations in present paper were performed at AFHB (Laboratories for IC-Engines and Exhaust Emission Control of the Berne University of Applied Sciences, Biel CH) as a part of the network project GasOMeP, together with the Swiss Research Institutions: EMPA, FHNW and PSI.

The objectives were to demonstrate the influences of increased lube oil consumption on the emissions, to show the effect of high quality exhaust gas filtration and to state if the different characteristics of lube oil will show measurable effects?

## 2. Test vehicle, fuel and lubricants

### 2.1 Test vehicle data

The tests on gasoline vehicle (GDI) were performed with a Seat Leon 1.4 TSI. This vehicle was operated with gasoline, in original condition (3WC) and with lube oil blended to the fuel, which simulated the increased lube oil consumption.

The vehicle is presented in Fig. 1 and Tab. 1.



Fig. 1. Seat Leon 1.4 TSI ST

Tab. 1. Technical data of tested vehicle

Model and year	Seat Leon 1.4 TSI ST/
Type of engine	CZEA
Number and arrangement of	4 / in line
Displacement	1395 cm <sup>3</sup>
Power	110 kW @ 6000 min <sup>-1</sup>
Torque	250 Nm @ 1500 min <sup>-1</sup>
Injection	Gasoline / DI
Turbocharging	Yes
Curb weight	1287 kg
Gross vehicle weight	1830 kg
Drive wheel	Front-wheel drive
Gearbox	m6
First registration / mileage	13.11.2014 / 27880 km
Exhaust standard	EURO 6b
Exhaust aftertreatment system	O <sub>2</sub> -Sonde, TWC

## 2.2 Fuel

The gasoline used was from the Swiss market, RON 95, according to SN EN228. A bigger charge of gasoline was purchased for the project and it was analyzed at INTERTEC Laboratory. The most important data are given in Table 2.

## 2.3 Lubricants

In the present tests the lube oil of the engine was not changed and analyzed – it was the lube oil recommended by the manufacturer Vapoil SAE 5W-30.

For the simulation of increased oil consumption by adding it to the fuel two other lube oils, manufactured and analysed at Motorex, CH, were used. See Table 3 for the results of analysis.

These lube oils were selected in order to enable the testing with high “H” ( $\leq 1.2\%$ ) or with low “L” ( $\leq 0.5\%$ ) content of ashes and metals. They have a unified HC-matrix (hydrocrack) and equal viscosity. This choice makes the influence of ashes and metals on the PN more visible.

Tab. 2. Data of gasoline

Property	Unit	Result
Density (at 15°C)	kg/m <sup>3</sup>	736.1
Vapor pressure (at 37.8°C)	kPa	67.3
Research Octan Number (RON)	-	95.6
Oxygen content	% (m/m)	1.0
Sulfur content	mg/kg	<1.0
Pb Lead	mg/L	<1.0
Ca Calcium	mg/kg	<1.0
Fe Iron	mg/kg	<1.0
Mg Magnesium	mg/kg	<1.0
Mn Manganese	mg/kg	<1.0
P Phosphorus	mg/kg	<1.0
Zn Zink	mg/kg	<1.0
Na Natrium	mg/kg	<1.0
K Potasium	mg/kg	<1.0
Distillation (at 101.3 kPa)		
• start	°C	34
• 10% Vol	°C	48
• 50% Vol	°C	75
• 90% Vol	°C	142
• end	°C	174

Tab. 3. Analysis data of the used lube oils

Property	“L” ACEA C4 SAE 5W/30	“H” ACEA A3/B4 SAE 5W/30	
Viscosity kin 40°C	68.5	69.7	mm <sup>2</sup> /s
Viscosity kin 100°C	11.96	11.90	mm <sup>2</sup> /s
Viscosity index	172.5	168.0	( --)
Density 20°C	852.4	855.0	kg/m <sup>3</sup>
Flamepoint	$\geq 200$	$\geq 200$	°C
Total Base Number	7.4	10.2	mg
Sulfur ashes	400	1200	mg/kg
Sulfur	1770	3376	mg/kg
Mg	21	66	mg/kg
Zn	517	1117	mg/kg
Ca	1219	3106	mg/kg
P	458	926	mg/kg
Sum S to P	3985	8591	mg/kg

## 3. Test methods and instrumentation

The vehicle was tested on a chassis dynamometer at constant speeds and in the dynamic driving cycles WLTC, with cold & warm engine.

The test series were:

- state of origin (gasoline, 3WC)
- addition of 2% lube oil “H” to fuel
- addition of 2% lube oil “H” to fuel + GPF
- addition of 2% lube oil “L” to fuel.

The driving resistances of the test bench were set according to the legal prescriptions, responding to the horizontal road.

The test equipment for regulated exhaust gas emissions (CO, HC, NO<sub>x</sub>, O<sub>2</sub>, CO<sub>2</sub>) fulfils the requirements of the Swiss and European exhaust gas legislation.

The dilution ratio DF in the CVS-dilution tunnel is variable and can be controlled by means of the CO<sub>2</sub>-analysis.

### 3.1 FTIR

FTIR (Fourier Transform Infrared) Spectrometer (AVL SESAM) offers the possibility of simultaneous, time-resolved measurement of approx. 30 emission components – among others: NO, NO<sub>2</sub>, NO<sub>x</sub>, NH<sub>3</sub>, N<sub>2</sub>O, HCN, HNCO, HCHO.

### 3.2 Nanoparticle analysis

The measurements of NP size distributions were conducted with different SMPS-systems, which enabled different ranges of size analysis:

SMPS: DMA TSI 3081 & CPC TSI 3772 (10-429 nm)

nSMPS: nDMA TSI 3085 & CPC TSI 3776 (2-64 nm).

For the dilution and sample preparation an ASET system from Matter Aerosol was used, (ASET ... aerosol sampling & evaporation tube). This system contains:

- Primary dilution air - MD19 tunable minidiluter (Matter Eng. MD19-2E).
- Secondary dilution air – dilution of the primary diluted and thermally conditioned measuring gas on the outlet of evaporative tube.
- Thermoconditioner (TC) - sample heating at 300°C.

In the tests the gas sample for the NP-analysis was taken from the undiluted exhaust gas at tailpipe for stationary operation (SMPS) or from the diluted exhaust gas in CVS-tunnel at transient operation (CPC).

### 3.5 Driving cycles

The steady state cycle (SSC) consists of 20 min-steps at 95, 61, 45, 26 km/h and idling, performed in the sequence from the highest to the lowest speed.

The approach to find a homogenized world-wide driving cycle was successfully finished with the development of the homogenized WLTP world-wide light duty test procedure. The WLTC (world-wide light duty test cycle) represents typical driving conditions around the world.

This cycle (Fig. 2) has been used also in this study. It represents different driving conditions: urban, rural, highway and extra-highway.

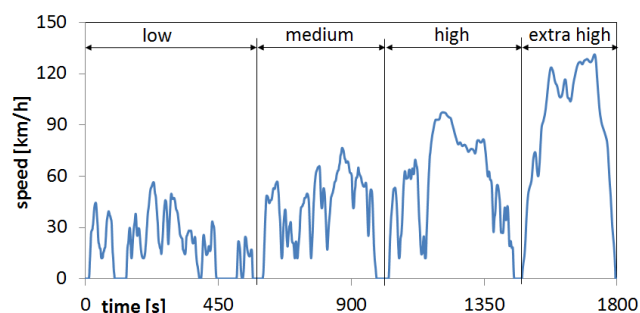


Fig. 2. WLTC driving cycle

## 4. Results

Fig. 3 represents the comparison of limited gaseous emissions CO, HC, and NO<sub>x</sub> in WLTC warm (averages of 3 cycles). The average emission levels with fuels containing lube oil are generally higher than the reference (gasoline). This is to explain with the higher content of heavy HC, their influence on chemistry of exhaust gases and on the Lambda regulation. There are, nevertheless, significant differences of CO- and HC-values between “2% H” and “2% H + GPF”. The questions arise: how repetitive are the CO peak values in WLTC? Can the GPF be responsible for the observed effects?

With this configuration (2% “H” + GPF) 30 WLTC with 3 cold starts were performed in the frame of another project. This gave the opportunity to consider the above questions. In Fig. 4 the peak CO-values, which were attained in the successive WLTC’s are represented. The values “cold start” are at the beginning of the cycles “1”, but the other peak values happen usually in the high speed / high acceleration periods of the cycle that means they are not dependent on the “cold start”. Also the “cold start” value from the 2nd day, which is represented in Fig. 4 seems to be exceptional. Finally, it can be stated, that the extreme CO-values are not connected to the GPF and they represent some coincidental and random states of the system (mixture preparation, λ-regulation, OBD-control, state of catalyst) of this vehicle. The influence of driver is unlikely, but cannot be excluded.

The results in SSC (not presented in this paper) confirm the highest CO & HC values with lube oil “H”.

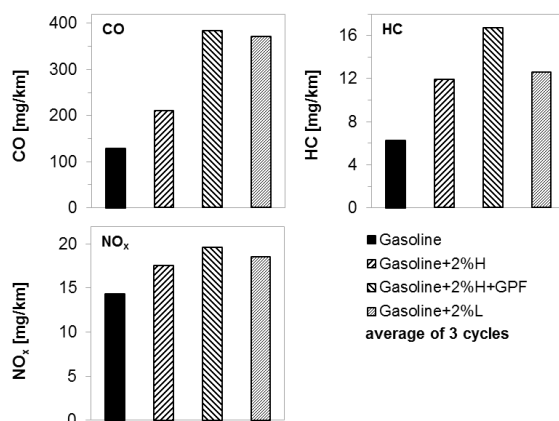


Fig. 3. Limited gaseous exhaust emissions in WLTC warm

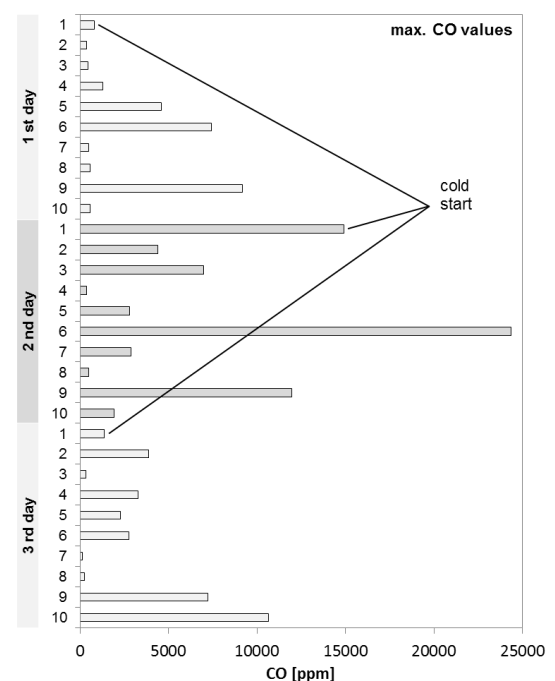


Fig. 4. Chronological comparison of CO peaks during 30 WLTC driving cycles. Fuel: gasoline + 2% oil H; with GPF

Fig. 5 compares the integral average values of non-legislated gaseous components in a single WLTC warm. There is a clear increase of NH<sub>3</sub> with fuels containing lube oil. This is a result from both influences: oil chemistry and impact of the oil on the Lambda regulation (more Lambda rich “excursions” provoke more NH<sub>3</sub>).

The emissions of NO<sub>2</sub>, N<sub>2</sub>O, HCHO and MeCHO are negligible.

In previous research of NH<sub>3</sub> emissions on gasoline vehicles, [19], was found that certain NH<sub>3</sub>-peaks in the repeated transient cycle (WLTC) appear randomly, while the NH<sub>3</sub>-peaks connected with the acceleration events in the high-speed part of the cycle appear regularly, but of course with an extremely varying intensity. This means that the NH<sub>3</sub>-emissions are irregular even in the repeating operating conditions. Additionally to the rich Lambda excursions and high exhaust temperatures further reasons for the NH<sub>3</sub>-fluctuations are the store/release effect of NH<sub>3</sub> and NH<sub>3</sub> precursor substances in the exhaust system and especially in the catalyst.

Considering this together with the emission variability represented in Fig. 4 the authors presume, that the NH<sub>3</sub> values in Fig. 5 are generally overlapped by the emission fluctuation.

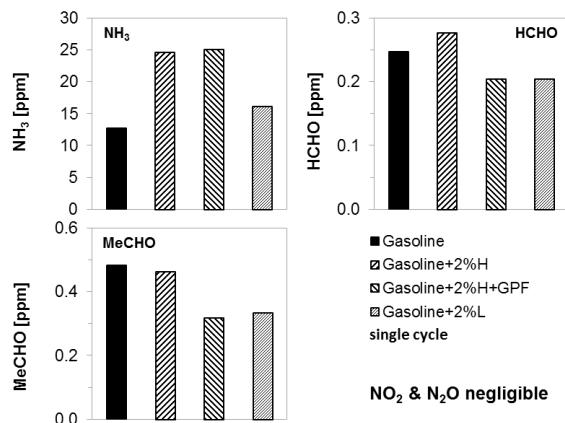


Figure 5: Non-legislated gaseous emissions in WLTC warm

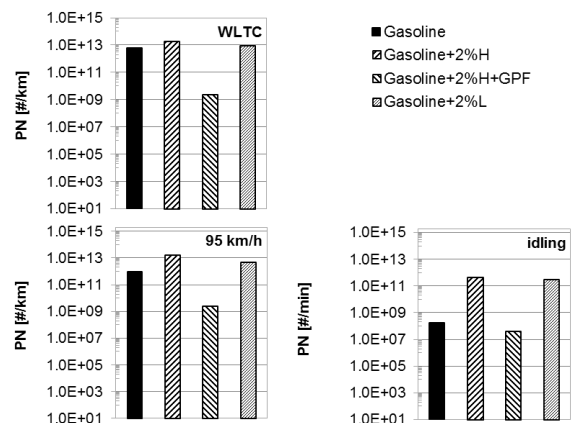


Figure 6: PN emissions during WLTC (3 cycles) and SSC (single) driving cycles warm

Fig. 6 represents the average PN-emission (WLTC averages of 3 cycles, SSC single cycle). It is demonstrated in this figure that the fuel variant “2% H” in-creases the nanoparticle emissions a little bit more than the fuel variant “2% L”. The applied, non-catalytic gasoline particle filter (GPF) eliminates very efficiently the nanoparticle counts.

Fig. 7 gives an exemplary comparison of SMPS particle size distribution (PSD) with the three fuel variants (gasoline, “H” and “L”).

SMPS size spectra with 2% lube oil “H” have maxima, which are by 1-2 orders of magnitude higher than in “state of reference” and these maxima are at lower sizes: example at 95 km/h maximum of PSD at 20nm, reference at 70nm. These are typical signs of nanoparticles originating from the lube oil, which was added to the fuel, like in the 2-stroke engines with lost oil lubrication.

Comparing the fuel variants “L” and “H” – there are tendencies of higher nuclei mode and lower sizes with lube oil “L” at 95 km/h. At 45 km/h and idling there are slightly lower peak values and lower median diameters. All that indicates the differences between the two lube oils “L” and “H”.

The progress of spontaneous condensation, which determinates the nuclei mode depends on the condensing substances, but also on the availability of condensation kernels. With the lube oil containing high amount of metals the probability of triggering the condensation is higher and bigger particle sizes can be developed.

At the bottom of Fig. 7 the total particle number (TPN) emissions in WLTC (averages of 3 cycles) are represented. This confirms the previous remarks that the lube oil “L” increases the PN-emissions less than the lube oil “H”.

Fig. 8 demonstrates an impressive reduction of particle count concentrations (SMPS at two chosen stationary operating points) and of TPN (in WLTC warm) by means of GPF.

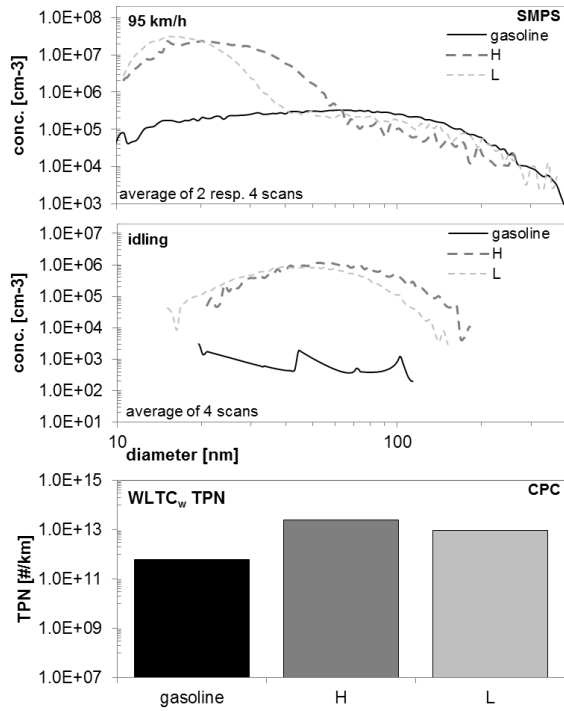


Fig. 7. Effect of increased lube consumption fuel: gasoline & gas. + 2% oil H... «high», L... «low» metals & ashes in lube oil

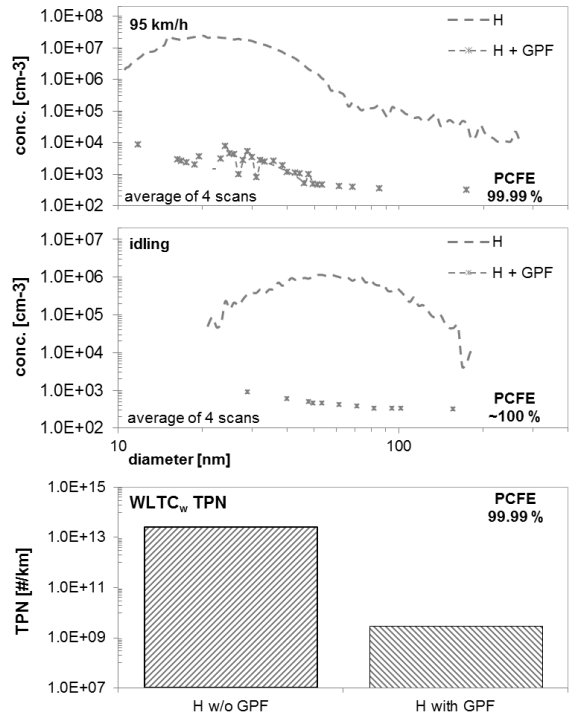


Fig. 8. Effect of GPF with increased lube oil consumption. Fuel: gasoline + 2% oil H; with & w/o GPF

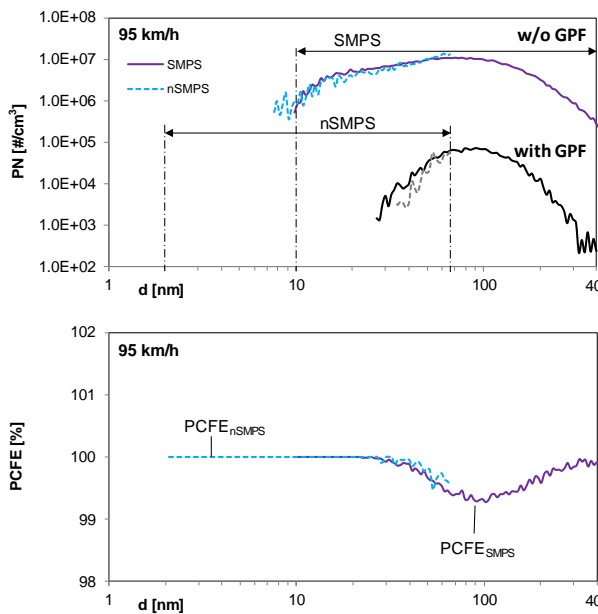


Fig. 9. Example of PSD's with SMPS & nSMPS and particle counts filtration efficiency (PCFE)

This reduction is by approximately 4 orders of magnitude and sets the particle count concentrations down to or below the ambient level.

The measurements of all PSD's at constant speeds were simultaneously performed with two systems SMPS (size range 10-429 nm) and nano-SMPS (size range 2-64 nm).

Generally there is a very good accordance of PSD's measured with both systems SMPS and nSMPS in the common size range (10-64 nm). Fig. 9 shows an example of scans with and without GPF. It confirms the excellent accordance of scans with both systems, it also confirms very good particle count filtration efficiency (PCFE) of the tested GPF and it particularly shows the total elimination of nanoparticles with sizes below 30 nm. In the whole test program there are no PC in the sizes below 6 nm and the PC in the size range 6 to 10 nm can be considered as negligible.

## 5. Conclusions

The obtained results allow following summarizing statements:

- the increased lube oil consumption increases emissions of CO and HC, it can have impact on Lambda regulation and contributes to increased NH<sub>3</sub>-values,
- with all fuels: gasoline, gasoline +”H” and gasoline +”L” there are no emissions of nitric dioxide NO<sub>2</sub>, of nitrous oxide N<sub>2</sub>O and negligible emissions (<1ppm) of aldehyde HCHO and of acetaldehyde MeOH,
- with increasing constant speed the NP-emissions increase for the investigated car; at idling there is the lowest NP-emission (1-2 orders of magnitude lower than with engine load),
- with addition of lube oil to the fuel (simulating the increased lube oil consumption) there is an increase of PN-emissions by approximately 2 orders of magnitude,
  - lube oil “H” increases PN by 2 orders of magnitude,
  - lube oil “L” increases PN a little less (1 to 1.5 orders of magnitude),
- the lube oil composition (HC-matrix and content of metals) influences slightly the particle size distributions,
- an efficient GPF eliminates the nanoparticles and lowers PN by 4 orders of magnitude.

## 6. Acknowledgements

The authors want to express their gratitude to the institutions, which financially supported the activities: Swiss Federal Office of Environment, Swiss Federal Office of Energy, Swiss Oil and Swiss Lubes.

## References

- [1] Sgro, L.A., et al., *Investigating the origin of nuclei particles in GDI engine exhaust*, Combustion and Flame, 2012. 159(4): p. 1687-1692.
- [2] Burtscher, H., *Physical characterization of particulate emissions from diesel engines*, a review. Journal of Aerosol Science, 2005. 36(7): p. 896-932.
- [3] Ulrich, A. and Wichser, A., *Analysis of additive metals in fuel and emission aerosols of diesel vehicles with and without particle traps*, Analytical and Bioanalytical Chemistry, 2003. 377(1): p. 71-81.
- [4] Hu, S., et al., *Metals emitted from heavy-duty diesel vehicles equipped with advanced PM and NO<sub>x</sub> emission controls*, Atmospheric Environment, 2009. 43(18): p. 2950-2959.
- [5] Mayer, A., Czerwinski, J.; Ulrich, A.; Mooney, J.J., *Metal-Oxide Particles in Combustion Engine Exhaust*, SAE Technical Paper 2010-01-0792.
- [6] Mayer, A.; Czerwinski, J.; Kasper, M.; Ulrich, A.; Mooney, J.J., *Metal Oxide Particle Emissions from Diesel and Petrol Engines*, SAE Technical Paper 2012-01-0841.
- [7] Ulrich, A., et al., *Particle and metal emissions of diesel and gasoline engines are particle filters appropriate measures?* Proceedings of the 16th ETH Conference on Combustion Generated Nanoparticles 2012.
- [8] Buchholz, B. A.; Dibble R. W.; Rich, D.; Cheng, A.S. (Ed)., *Quantifying the contribution of lubrication oil carbon to particulate emissions from a diesel engine*, SAE Technical Paper 2003-01-1987.
- [9] Sonntag, D. B.; Bailey, Ch. R.; Fulper, C. R.; Baldauf, R.W., *Contribution of Lubricating Oil to Particulate Matter Emissions from Light-Duty Gasoline Vehicles in Kansas City*, Environment Science & Technology, 27. Febr. 2012.



- [10] Hadler, J.; Lensch-Franze, Ch.; Gohl, M.; Mink, T., *Emission Reduction A Solution of Lubricant Composition, Calibration and Mechanical Development*, MTZ, September 2015.
- [11] Yinhui, W.; Rong, Z.; Yanhong, Q.; Jianfei, P.; Mengren, L.; Jianrong, L.; Yusheng, W.; Min, H.; Shijin, S., *The impact of fuel compositions on the particulate emissions of direct injection gasoline engine*, Elsevier, Fuel 166 (2016) 543-552. Journal homepage: [www.elsevier.com/locate/fuel](http://www.elsevier.com/locate/fuel).
- [12] Bach, C., *Emissionsvergleich verschiedener Antriebsarten in aktuellen Personenwagen*, Untersuchung der Emissionen von aktuellen Personenwagen mit konventionellen und direkteingespritzten Benzinmotoren, Dieselmotoren mit und ohne Partikelfilter, sowie Erdgasmotoren, (Empa Final Report for Novatlantis and Bundesamt für Umwelt BAFU), in Empa Report 2007 (Novatlantis).
- [13] Bielaczyc, P.; Szczotka, A.; Woodburn, J., *An overview of particulate matter emissions from modern light duty vehicles*, Combustion Engines, No. 2/2013 (153), 101-108. ISSN 0138-0346.
- [14] Chan, T.W.; Meloche, E.; Kubsh, J.; Brezny, R.; Rosenblatt, D.; Rideout, G., *Impact of Ambient Temperature on Gaseous and Particle Emissions from a Direct Injection Gasoline Vehicle and its Implications on Particle Filtration*, SAE Technical Paper 2013-01-0527, Detroit, April 2013.

## Abbreviations

AFHB	Abgasprüfstelle FH Biel, CH	NH <sub>3</sub>	Ammonia
ASET	Aerosol Sampling & Evaporation Tube	NO <sub>x</sub>	nitric oxides
BAFU	Bundesamt für Umwelt, (see FOEN)	NP	nanoparticles < 999 nm
CLA	chemiluminescent analyzer	nSMPS	nano SMPS
CPC	condensation particle counter	PC	particle counts (integrated)
CVS	constant volume sampling	PCFE	particle counts filtration efficiency
DF	dilution factor	PM	particle mass
DI	Direct Injection	PN	particle numbers
DMA	differential mobility analyzer	PSD	particle size distribution
EGR	exhaust gas recirculation	PSI	Paul Scherrer Institute
EMPA	Eidgenössische Material Prüf- und Forschungsanstalt	SMPS	scanning mobility particle sizer
FHNW	Fachhochschule Nord-West Schweiz	TC	thermoconditioner
FOEN	Federal Office for Environment	TPN	total particle numbers
GasOMeP	Gasoline Organic & Metal Particles	TTM	Technik Thermische Maschinen
GDI	gasoline direct injection	TWC	three way catalyst
GPF	gasoline particle filter	VERT	Verification of Emission Reduction Technologies (VERT Association)
„H“	high (ash/metal content)	WLTC	Worldwide Light Duty Test Cycle
HCHO	Formaldehyde	3WC	three way catalyst
„L“	low (ash/metal content)		
MD	minidiluter		
MeCHO	Acetaldehyde		
NO	nitrogen monoxide		
NO <sub>2</sub>	nitrogen dioxide		
N <sub>2</sub> O	nitrous oxide		